

BoltGroup Verification Manual

This following document compares BoltGroup analysis results with the tabulated method provided in AISC. Tables 7-7 through 7-14 employ the instantaneous center of rotation method for the bolt patterns and eccentric conditions indicated, and inclined loads at 0°, 15°, 30°, 45°, 60°, and 75°. The tabulated non-dimensional coefficient, C , represents the number of bolts that are effective in resisting the eccentric shear force.

$$\phi R_n = \phi C \times r_n$$

where

C = tabular value

r_n = nominal strength per bolt, kip

ϕ = 0.75

Example 1

Determine available strength of bolt group connection with five bolts in each of two vertical rows (2 x 5). Vertical bolt spacing $S = 3$ inches, horizontal bolt spacing 3 inches, 7/8" diameter A325N bolts are loaded in shear, $\phi_v r_n = 21.6$ kip (Table 7-1). The in-plane resultant force $P = 70$ kips is inclined 30° and applied with eccentricity $e_x = 10$ inches.

- a) Using BoltGroup spreadsheet $\phi R_n = \mathbf{83.48}$ kips
- b) Using AISC table 7-8
 $C(e_x=10", S=3", n=5) = 3.87$
 $\phi R_n = \phi C r_n = 3.87(21.6) = \mathbf{83.59}$ kips
- c) BoltGroup Deviation = $(83.59-83.48)/83.59 = \mathbf{0.13\%}$

Example 2

Determine available strength of bolt group connection with nine bolts in each of two vertical rows (2 x 9). Vertical bolt spacing $S = 6$ inches, horizontal bolt spacing 3 inches, 7/8" diameter A325N bolts are loaded in shear, $\phi_v r_n = 21.6$ kip (Table 7-1). The in-plane resultant force $P = 140$ kips is inclined 30° and applied with eccentricity $e_x = 28$ inches.

- a) Using BoltGroup spreadsheet $\phi R_n = \mathbf{172.60}$ kips
- b) Using AISC table 7-8
 $C(e_x=10", S=3", n=5) = 7.99$
 $\phi R_n = \phi C r_n = 7.99(21.6) = \mathbf{172.58}$ kips
- c) BoltGroup Deviation = $(172.58-172.60)/172.58 = \mathbf{-0.01\%}$

| | | | | |
|-------------------------------|---|-----------|--------|-----------|
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| | | Date: | 12-Apr | |
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| | | Date: | | |

ECCENTRICALLY LOADED BOLT GROUP ANALYSIS

The following calculations comply with AISC Manual 13th Edition

Units:

Applied Forces

| Start Location | | Direction | Value |
|----------------|----|-----------|-------|
| X | Y | β | P |
| in | in | deg | kip |
| 10 | 0 | -120 | 70 |

Force Resultant: Total force $P_u = 70.00$ kip
 $P_x = \sum P \cos(\beta) = -35.00$ kip
 $P_y = \sum P \sin(\beta) = -60.62$ kip
 $\beta = -120.00$ deg
Moment about CG, $M_{CG} = -606.22$ kip-in
Eccentricity to CG, $e = M_{CG}/P_u = -8.66$ in
 $X_p = X_c + e \sin(\beta) = 7.500$ in
 $Y_p = Y_c - e \cos(\beta) = -4.330$ in

Bolt Group: Nbolts = 10 (< 100)
Center Gravity (CG) Instantaneous Center (IC)
 $X_c = 0$ in $X_{IC} = -1.71248$ in
 $Y_c = 0$ in $Y_{IC} = 1.55371$ in

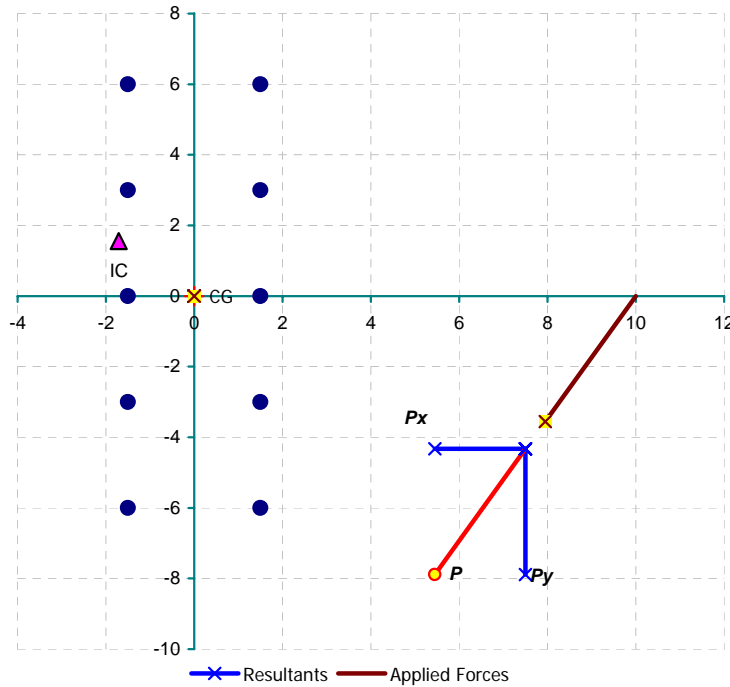
Bolt group shear capacity:
LRFD method: $\phi P = 83.48$ kip >= 70 OK
Elastic method: $\phi P = 63.22$ kip < 70 N.G. Solved !

Add torque = kip-in

Bolt type:

Bolt capacity $\phi R_n = 21.6$ kip

| Bolt Location | | |
|---------------|------|----|
| Bolt No. | X | Y |
| (<= 100) | in | in |
| 1 | -1.5 | 6 |
| 2 | -1.5 | 3 |
| 3 | -1.5 | 0 |
| 4 | -1.5 | -3 |
| 5 | -1.5 | -6 |
| 6 | 1.5 | -6 |
| 7 | 1.5 | 6 |
| 8 | 1.5 | 3 |
| 9 | 1.5 | 0 |
| 10 | 1.5 | -3 |



| | | | | |
|-----------------------------|---|-------------------------------------|--------------|-----------|
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ECCENTRICALLY LOADED BOLT GROUP ANALYSIS

The following calculations comply with AISC Manual 13th Edition

Units:

Applied Forces

| Start Location | | Direction | Value |
|----------------|----|-----------|-------|
| X | Y | β | P |
| in | in | deg | kip |
| 28 | 0 | -120 | 140 |

Force Resultant: Total force $P_u = 140.00$ kip
 $P_x = \sum P \cos(\beta) = -70.00$ kip
 $P_y = \sum P \sin(\beta) = -121.24$ kip
 $\beta = -120.00$ deg
Moment about CG, $M_{CG} = -3394.82$ kip-in
Eccentricity to CG, $e = M_{CG}/P_u = -24.25$ in
 $X_p = X_c + e \sin(\beta) = 21.000$ in
 $Y_p = Y_c - e \cos(\beta) = -12.124$ in

Bolt Group: Nbolts = 18 (< 100)
Center Gravity (CG) Instantaneous Center (IC)
 $X_c = 0$ in $X_{IC} = -5.96291$ in
 $Y_c = 0$ in $Y_{IC} = 6.3331$ in

Bolt group shear capacity:
LRFD method: $\phi P = 172.60$ kip ≥ 140 OK
Elastic method: $\phi P = 126.43$ kip < 140 N.G. Solved!

Add torque = kip-in

Bolt type:

Bolt capacity $\phi R_n = 21.6$ kip

| Bolt Location | | |
|----------------|------|-----|
| Bolt No. | X | Y |
| (≤ 100) | in | in |
| 1 | -1.5 | 24 |
| 2 | -1.5 | 18 |
| 3 | -1.5 | 12 |
| 4 | -1.5 | 6 |
| 5 | -1.5 | 0 |
| 6 | -1.5 | -6 |
| 7 | -1.5 | -12 |
| 8 | -1.5 | -18 |
| 9 | -1.5 | -24 |
| 10 | 1.5 | 24 |
| 11 | 1.5 | 18 |
| 12 | 1.5 | 12 |
| 13 | 1.5 | 6 |
| 14 | 1.5 | 0 |
| 15 | 1.5 | -6 |
| 16 | 1.5 | -12 |
| 17 | 1.5 | -18 |
| 18 | 1.5 | -24 |

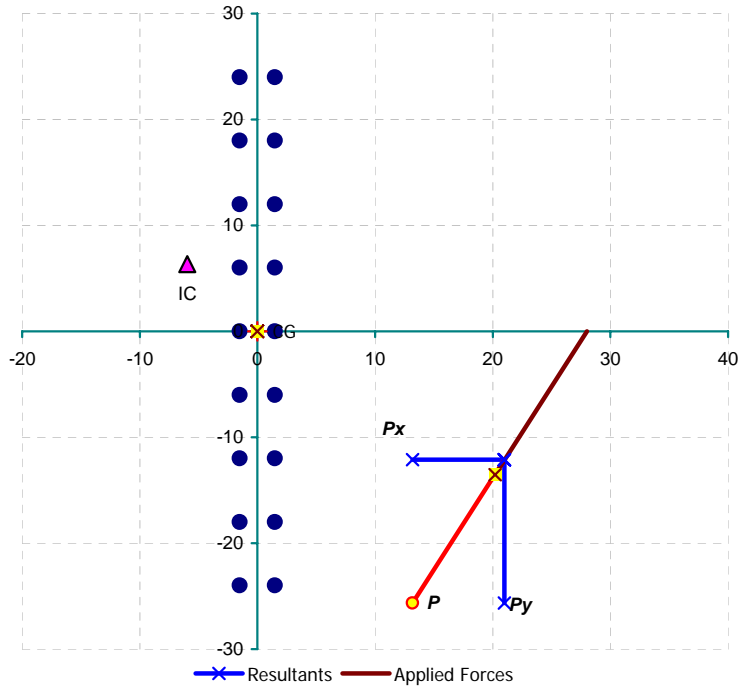


Table 7-8 (continued)

Coefficients C for Eccentrically Loaded Bolt Groups
Angle = 30°

Available Strength of a bolt group, ϕR_n or R_n/Ω , is determined with

$$R_n = C \times r_n$$

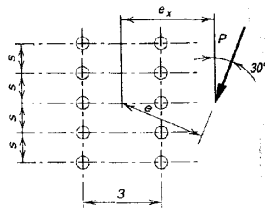
$$\phi = 0.75 \quad \Omega = 2.00$$

or

| LRFD | ASD |
|----------------------------------|------------------------------------|
| $C_{min} = \frac{P_u}{\phi r_n}$ | $C_{min} = \frac{\Omega P_a}{r_n}$ |

where

- P = required force, P_u or P_a , kips
- r_n = nominal strength per bolt, kips
- e = eccentricity of P with respect to centroid of bolt group, in. (not tabulated, may be determined by geometry)
- e_x = horizontal component of e , in.
- s = bolt spacing, in.
- C = coefficient tabulated below



Number of Bolts in One Vertical Row, n

| s , in. | e_x , in. | Number of Bolts in One Vertical Row, n | | | | | | | | | | | |
|-----------|-------------|--|------|------|------|------|------|------|------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 3 | 2 | 0.97 | 2.60 | 4.52 | 6.54 | 8.59 | 10.6 | 12.7 | 14.7 | 16.7 | 18.8 | 20.8 | 22.8 |
| | 3 | 0.75 | 2.12 | 3.83 | 5.71 | 7.71 | 9.75 | 11.8 | 13.9 | 15.9 | 18.0 | 20.0 | 22.1 |
| | 4 | 0.62 | 1.78 | 3.29 | 4.99 | 6.88 | 8.87 | 10.9 | 13.0 | 15.1 | 17.1 | 19.2 | 21.3 |
| | 5 | 0.52 | 1.53 | 2.85 | 4.39 | 6.16 | 8.06 | 10.0 | 12.1 | 14.1 | 16.2 | 18.3 | 20.4 |
| | 6 | 0.45 | 1.34 | 2.51 | 3.89 | 5.54 | 7.33 | 9.23 | 11.2 | 13.2 | 15.3 | 17.3 | 19.4 |
| | 7 | 0.40 | 1.19 | 2.23 | 3.48 | 5.01 | 6.70 | 8.51 | 10.4 | 12.4 | 14.4 | 16.4 | 18.5 |
| | 8 | 0.36 | 1.07 | 2.00 | 3.15 | 4.57 | 6.14 | 7.86 | 9.68 | 11.6 | 13.6 | 15.6 | 17.6 |
| | 9 | 0.32 | 0.97 | 1.81 | 2.87 | 4.19 | 5.66 | 7.28 | 9.02 | 10.9 | 12.8 | 14.7 | 16.7 |
| | 10 | 0.30 | 0.88 | 1.66 | 2.64 | 3.87 | 5.24 | 6.77 | 8.43 | 10.2 | 12.0 | 13.9 | 15.9 |
| | 12 | 0.25 | 0.75 | 1.41 | 2.27 | 3.34 | 4.54 | 5.92 | 7.43 | 9.04 | 10.8 | 12.5 | 14.4 |
| | 14 | 0.22 | 0.65 | 1.23 | 1.98 | 2.93 | 3.99 | 5.24 | 6.61 | 8.09 | 9.67 | 11.4 | 13.1 |
| | 16 | 0.19 | 0.58 | 1.08 | 1.76 | 2.60 | 3.56 | 4.69 | 5.94 | 7.30 | 8.77 | 10.3 | 12.0 |
| | 18 | 0.17 | 0.52 | 0.97 | 1.58 | 2.34 | 3.21 | 4.24 | 5.38 | 6.64 | 8.0 | 9.45 | 11.0 |
| | 20 | 0.16 | 0.47 | 0.88 | 1.43 | 2.12 | 2.92 | 3.87 | 4.92 | 6.08 | 7.3 | 8.70 | 10.1 |
| | 24 | 0.13 | 0.39 | 0.74 | 1.21 | 1.79 | 2.48 | 3.29 | 4.18 | 5.19 | 6.3 | 7.48 | 8.75 |
| | 28 | 0.12 | 0.34 | 0.64 | 1.04 | 1.55 | 2.14 | 2.85 | 3.63 | 4.52 | 5.5 | 6.54 | 7.68 |
| 32 | 0.10 | 0.30 | 0.56 | 0.92 | 1.36 | 1.89 | 2.51 | 3.21 | 4.00 | 4.9 | 5.81 | 6.83 | |
| 36 | 0.09 | 0.26 | 0.50 | 0.82 | 1.21 | 1.69 | 2.25 | 2.87 | 3.59 | 4.4 | 5.22 | 6.15 | |
| 6 | 2 | 0.97 | 3.20 | 5.31 | 7.37 | 9.39 | 11.4 | 13.4 | 15.4 | 17.4 | 19.4 | 21.3 | 23.3 |
| | 3 | 0.75 | 2.75 | 4.86 | 6.95 | 9.01 | 11.1 | 13.1 | 15.1 | 17.1 | 19.1 | 21.1 | 23.1 |
| | 4 | 0.62 | 2.39 | 4.42 | 6.49 | 8.57 | 10.6 | 12.7 | 14.7 | 16.8 | 18.8 | 20.8 | 22.8 |
| | 5 | 0.52 | 2.10 | 4.02 | 6.04 | 8.11 | 10.2 | 12.3 | 14.3 | 16.4 | 18.4 | 20.4 | 22.5 |
| | 6 | 0.45 | 1.87 | 3.67 | 5.61 | 7.66 | 9.73 | 11.8 | 13.9 | 16.0 | 18.0 | 20.1 | 22.1 |
| | 7 | 0.40 | 1.69 | 3.36 | 5.21 | 7.21 | 9.27 | 11.4 | 13.4 | 15.5 | 17.6 | 19.6 | 21.7 |
| | 8 | 0.36 | 1.53 | 3.08 | 4.84 | 6.79 | 8.82 | 10.9 | 13.0 | 15.1 | 17.1 | 19.2 | 21.3 |
| | 9 | 0.32 | 1.40 | 2.84 | 4.51 | 6.40 | 8.39 | 10.4 | 12.5 | 14.6 | 16.7 | 18.7 | 20.8 |
| | 10 | 0.30 | 1.29 | 2.63 | 4.21 | 6.04 | 7.98 | 9.99 | 12.0 | 14.1 | 16.2 | 18.3 | 20.4 |
| | 12 | 0.25 | 1.12 | 2.28 | 3.70 | 5.39 | 7.23 | 9.16 | 11.2 | 13.2 | 15.3 | 17.3 | 19.4 |
| | 14 | 0.22 | 0.98 | 2.00 | 3.29 | 4.86 | 6.57 | 8.41 | 10.3 | 12.3 | 14.4 | 16.4 | 18.5 |
| | 16 | 0.19 | 0.87 | 1.78 | 2.95 | 4.40 | 6.01 | 7.75 | 9.6 | 11.5 | 13.5 | 15.5 | 17.6 |
| | 18 | 0.17 | 0.79 | 1.60 | 2.68 | 4.02 | 5.52 | 7.17 | 8.9 | 10.8 | 12.7 | 14.7 | 16.7 |
| | 20 | 0.16 | 0.71 | 1.45 | 2.45 | 3.70 | 5.09 | 6.65 | 8.3 | 10.1 | 12.0 | 13.9 | 15.9 |
| | 24 | 0.13 | 0.60 | 1.23 | 2.08 | 3.17 | 4.39 | 5.79 | 7.3 | 8.95 | 10.7 | 12.5 | 14.4 |
| | 28 | 0.12 | 0.52 | 1.06 | 1.82 | 2.77 | 3.85 | 5.11 | 6.5 | 7.99 | 9.59 | 11.3 | 13.0 |
| 32 | 0.10 | 0.46 | 0.93 | 1.61 | 2.45 | 3.42 | 4.56 | 5.8 | 7.20 | 8.68 | 10.3 | 11.9 | |
| 36 | 0.09 | 0.41 | 0.83 | 1.44 | 2.20 | 3.08 | 4.12 | 5.3 | 6.53 | 7.91 | 9.37 | 10.9 | |

Example 3

Determine available strength of bolt group connection with three bolts in each of three vertical rows (3 x 3). Vertical bolt spacing $S = 6$ inches, horizontal bolt spacing 6 inches, 7/8" diameter A325N bolts are loaded in shear, $\phi_v r_n = 21.6$ kip (Table 7-1). The in-plane resultant force $P = 100$ kips is inclined 75° and applied with eccentricity $e_x = 20$ inches.

a) Using BoltGroup spreadsheet $\phi R_n = 132.85$ kips

b) Using AISC table 7-12

$$C(e_x=20", S=6", n=3) = 6.15$$

$$\phi R_n = \phi C r_n = 6.15(21.6) = 132.84 \text{ kips}$$

c) BoltGroup Deviation = -0.0075%

| | | | | |
|-------------------------------|---|--------------------|--------------|-----------|
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ECCENTRICALLY LOADED BOLT GROUP ANALYSIS

The following calculations comply with AISC Manual 13th Edition

Units:

Applied Forces

| Start Location | | Direction | Value |
|----------------|----|-----------|-------|
| X | Y | β | P |
| in | in | deg | kip |
| 20 | 0 | -165 | 80 |

Force Resultant: Total force $P_u = 80.00$ kip
 $P_x = \sum P \cos(\beta) = -77.27$ kip
 $P_y = \sum P \sin(\beta) = -20.71$ kip
 $\beta = -165.00$ deg
Moment about CG, $M_{CG} = -414.11$ kip-in
Eccentricity to CG, $e = M_{CG}/P_u = -5.18$ in
 $X_p = X_c + e \sin(\beta) = 1.340$ in
 $Y_p = Y_c - e \cos(\beta) = -5.000$ in

Bolt Group: Nbolts = 9 (< 100)
Center Gravity (CG) Instantaneous Center (IC)
 $X_C = 0$ in $X_{IC} = -2.11599$ in
 $Y_C = 0$ in $Y_{IC} = 7.67525$ in

Bolt group shear capacity:
LRFD method: $\phi P = 132.85$ kip > = 80 OK
Elastic method: $\phi P = 105.08$ kip > = 80 OK Solved !

Add torque = kip-in

Bolt type:

Bolt capacity $\phi R_n = 21.6$ kip

| Bolt Location | | |
|---------------|----|----|
| Bolt No. | X | Y |
| (<= 100) | in | in |
| 1 | -6 | 6 |
| 2 | -6 | 0 |
| 3 | -6 | -6 |
| 4 | 0 | 6 |
| 5 | 0 | 0 |
| 6 | 0 | -6 |
| 7 | 6 | 6 |
| 8 | 6 | 0 |
| 9 | 6 | -6 |

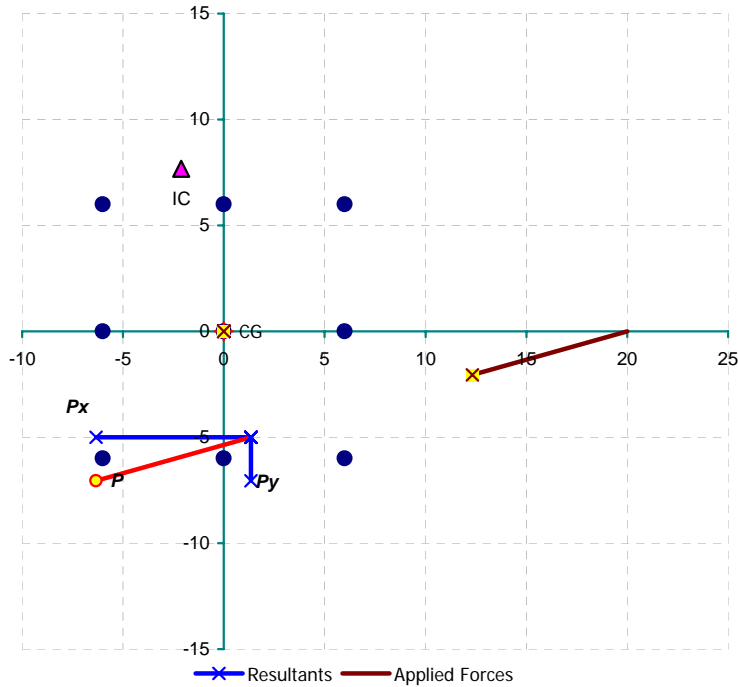


Table 7-12 (continued)

Coefficients C for Eccentrically Loaded Bolt Groups

Angle = 75°

Available Strength of a bolt group, ϕR_n or R_n/Ω , is determined with

$$R_n = C \times r_n$$

$$\phi = 0.75 \quad \Omega = 2.00$$

or

| LRFD | ASD |
|----------------------------------|------------------------------------|
| $C_{min} = \frac{P_u}{\phi R_n}$ | $C_{min} = \frac{\Omega P_a}{r_n}$ |

where

P = required force, P_u or P_a , kips

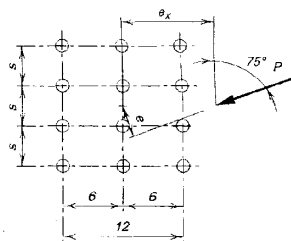
r_n = nominal strength per bolt, kips

e = eccentricity of P with respect to centroid of bolt group, in.
(not tabulated, may be determined by geometry)

e_x = horizontal component of e , in.

s = bolt spacing, in.

C = coefficient tabulated below



| s, in. | e_x , in. | Number of Bolts in One Vertical Row, n | | | | | | | | | | | |
|--------|-------------|--|------|------|------|------|------|------|------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 3 | 2 | 2.92 | 5.83 | 8.73 | 11.6 | 14.5 | 17.4 | 20.3 | 23.1 | 26.0 | 28.9 | 31.8 | 34.7 |
| | 3 | 2.89 | 5.77 | 8.63 | 11.5 | 14.3 | 17.2 | 20.0 | 22.8 | 25.7 | 28.5 | 31.4 | 34.2 |
| | 4 | 2.86 | 5.70 | 8.51 | 11.3 | 14.1 | 16.9 | 19.7 | 22.5 | 25.3 | 28.1 | 30.9 | 33.7 |
| | 5 | 2.82 | 5.61 | 8.38 | 11.1 | 13.9 | 16.6 | 19.4 | 22.1 | 24.9 | 27.7 | 30.5 | 33.3 |
| | 6 | 2.77 | 5.51 | 8.23 | 10.9 | 13.6 | 16.3 | 19.0 | 21.8 | 24.5 | 27.2 | 30.0 | 32.8 |
| | 7 | 2.72 | 5.40 | 8.06 | 10.7 | 13.4 | 16.0 | 18.7 | 21.4 | 24.1 | 26.8 | 29.6 | 32.3 |
| | 8 | 2.66 | 5.29 | 7.89 | 10.5 | 13.1 | 15.7 | 18.3 | 21.0 | 23.7 | 26.4 | 29.1 | 31.9 |
| | 9 | 2.60 | 5.16 | 7.71 | 10.3 | 12.8 | 15.4 | 18.0 | 20.6 | 23.3 | 26.0 | 28.7 | 31.4 |
| | 10 | 2.53 | 5.04 | 7.53 | 10.0 | 12.6 | 15.1 | 17.7 | 20.3 | 22.9 | 25.6 | 28.3 | 31.0 |
| | 12 | 2.40 | 4.78 | 7.16 | 9.57 | 12.0 | 14.5 | 17.0 | 19.6 | 22.1 | 24.8 | 27.4 | 30.1 |
| | 14 | 2.26 | 4.52 | 6.80 | 9.12 | 11.5 | 13.9 | 16.4 | 18.9 | 21.4 | 24.0 | 26.6 | 29.3 |
| | 16 | 2.13 | 4.27 | 6.45 | 8.68 | 11.0 | 13.3 | 15.8 | 18.2 | 20.7 | 23.3 | 25.9 | 28.5 |
| | 18 | 2.00 | 4.03 | 6.12 | 8.27 | 10.5 | 12.8 | 15.2 | 17.6 | 20.1 | 22.6 | 25.1 | 27.7 |
| | 20 | 1.89 | 3.81 | 5.80 | 7.88 | 10.1 | 12.3 | 14.6 | 17.0 | 19.4 | 21.9 | 24.4 | 27.0 |
| 24 | 1.67 | 3.41 | 5.24 | 7.18 | 9.22 | 11.4 | 13.6 | 15.9 | 18.2 | 20.7 | 23.1 | 25.6 | |
| 28 | 1.49 | 3.06 | 4.75 | 6.56 | 8.49 | 10.5 | 12.6 | 14.9 | 17.1 | 19.5 | 21.9 | 24.3 | |
| 32 | 1.34 | 2.77 | 4.33 | 6.02 | 7.84 | 9.77 | 11.8 | 13.9 | 16.1 | 18.4 | 20.7 | 23.1 | |
| 36 | 1.21 | 2.52 | 3.97 | 5.56 | 7.27 | 9.10 | 11.1 | 13.1 | 15.2 | 17.4 | 19.7 | 22.0 | |
| 6 | 2 | 2.92 | 5.82 | 8.71 | 11.6 | 14.5 | 17.4 | 20.3 | 23.5 | 26.4 | 29.3 | 32.3 | 35.2 |
| | 3 | 2.89 | 5.76 | 8.60 | 11.4 | 14.3 | 17.1 | 20.0 | 22.9 | 25.8 | 28.7 | 31.7 | 34.6 |
| | 4 | 2.86 | 5.68 | 8.47 | 11.3 | 14.1 | 16.9 | 19.8 | 22.6 | 25.5 | 28.4 | 31.3 | 34.2 |
| | 5 | 2.82 | 5.59 | 8.34 | 11.1 | 13.9 | 16.7 | 19.5 | 22.4 | 25.2 | 28.1 | 31.0 | 33.9 |
| | 6 | 2.77 | 5.49 | 8.19 | 10.9 | 13.7 | 16.4 | 19.2 | 22.1 | 24.9 | 27.8 | 30.7 | 33.6 |
| | 7 | 2.72 | 5.39 | 8.04 | 10.7 | 13.4 | 16.2 | 19.0 | 21.8 | 24.6 | 27.5 | 30.4 | 33.3 |
| | 8 | 2.66 | 5.27 | 7.89 | 10.5 | 13.2 | 16.0 | 18.8 | 21.6 | 24.4 | 27.2 | 30.1 | 33.0 |
| | 9 | 2.60 | 5.16 | 7.74 | 10.4 | 13.0 | 15.8 | 18.5 | 21.3 | 24.1 | 27.0 | 29.8 | 32.7 |
| | 10 | 2.53 | 5.04 | 7.58 | 10.2 | 12.8 | 15.5 | 18.3 | 21.0 | 23.9 | 26.7 | 29.5 | 32.4 |
| | 12 | 2.40 | 4.81 | 7.27 | 9.81 | 12.4 | 15.1 | 17.8 | 20.6 | 23.3 | 26.2 | 29.0 | 31.8 |
| | 14 | 2.26 | 4.57 | 6.97 | 9.47 | 12.0 | 14.7 | 17.4 | 20.1 | 22.9 | 25.6 | 28.4 | 31.3 |
| | 16 | 2.13 | 4.35 | 6.69 | 9.13 | 11.7 | 14.3 | 16.9 | 19.6 | 22.4 | 25.1 | 27.9 | 30.7 |
| | 18 | 2.00 | 4.13 | 6.41 | 8.82 | 11.3 | 13.9 | 16.5 | 19.2 | 21.9 | 24.7 | 27.4 | 30.2 |
| | 20 | 1.89 | 3.93 | 6.15 | 8.51 | 11.0 | 13.5 | 16.1 | 18.8 | 21.5 | 24.2 | 27.0 | 29.8 |
| 24 | 1.67 | 3.57 | 5.67 | 7.95 | 10.4 | 12.9 | 15.4 | 18.0 | 20.7 | 23.4 | 26.1 | 28.8 | |
| 28 | 1.49 | 3.25 | 5.25 | 7.44 | 9.77 | 12.2 | 14.7 | 17.3 | 19.9 | 22.6 | 25.3 | 28.0 | |
| 32 | 1.34 | 2.97 | 4.87 | 6.98 | 9.23 | 11.6 | 14.1 | 16.6 | 19.2 | 21.8 | 24.5 | 27.2 | |
| 36 | 1.21 | 2.73 | 4.54 | 6.56 | 8.74 | 11.1 | 13.5 | 16.0 | 18.5 | 21.1 | 23.7 | 26.4 | |